# DEFORMATION OF YULE MARBLE: PART IV-EFFECTS AT 150°C.

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## ABSTRACT

Yule marble has been experimentally deformed at  $150^{\circ}$ C under conditions otherwise identical with those at room temperature reported in Part I. The strength is lowered about 40 per cent by this increase in temperature, and the relative ease of translation versus twinning on  $\{01\overline{1}2\}$  is increased. Fabric measurements on the deformed material show trends nearly identical with those at room temperature (Part III). The individual grains are more homogeneously deformed, and, perhaps as a consequence, the fabric changes appear to be somewhat more sharply defined. Effects of interstitial water and of slow rate of deformation are negligible except for a lowering of strength similar to that observed at room temperature. The fabric changes are completely consistent with those predicted in Part II under the hypothesis of homogeneous deformation. By all tests applied, the mechanism of deformation is thus the same as at room temperature, and is dominantly twinning and translation on  $\{01\overline{1}2\}$ . The observed lowering in strength and greater homogeneity of texture suggest an approach to conditions of natural deformation.

## CONTENTS

1

1

Page

Figure

## TEXT

	-
Introduction	1385
Acknowledgments	1380
Experiments	1380
Âpparatus	1380
Procedure	1380
Results	1387
Miscellaneous effects.	1392
Summary of experimental results	1393
Fabric of deformed marble	1393
Material for study	1393
General microscopic character of fabric	1393
Petrofabric analysis	1395
Procedure	1395
Preferred orientation of optic axis $c$	1395
Preferred orientation of best developed	
{0112} lamellae	1398
Preferred orientation of edges [e:e]	1398
Influence of temperature, water, time on	
deformed fabric	1404
Temperature	1404
Water	1404
Time	1404
Conclusion	1404
References cited	1403

## ILLUSTRATIONS

riguie	ige
1. Stress-strain curves of Yule marble 13	88
2. Stress-strain curves of calcite single crys- tals	389

#### INTRODUCTION

Parts I, II, and III of this paper (Griggs and Miller, 1951; Handin and Griggs, 1951;

in a calcite grain	1394
6. Orientation diagrams for c axes of calcite	107
in undeformed Vule marble	1390
7. Orientation diagrams for c axes of calcite	1070
in deformed Vule marble	1.397
8. Pairs of c axes for twinned grains of calcite	1398
9. Orientation diagrams for best-developed	
{0112} lamellae in calcite of deformed	
Yule marble.	1399
0. Orientation diagrams for edges [e:e] in	
calcite of deformed Yule marble	1400
1. Idealized orientation diagrams showing	
maxima for $c$ axes, $\{01\overline{1}2\}$ lamellae, and	
[e:e] edges, in relation to applied stress	
and pre-deformational fabric	1401
2. Comparison of fabrics of marbles deformed	
dry and in water at 150°C	1402
3. Comparison of fabrics of marbles deformed	
rapidly and slowly at 150°C in water	1403
TADIES	
TABLES	
Cable	Page
. Test of homogeneous hypothesis on 150°C.	
dry data	1389
2. Test of homogeneous hypothesis on 150°C	
wet data	1391
. Effect of confining pressure on stress-strain	
characteristics	1392
. Specimens subjected to fabric analysis	1393

3. Effect of varying amounts of water ..... 1390

4. Effect of different rates of strain .....

5. Acutely intersecting lamellae e and e

Page

1391

Turner and Ch'ih, 1951) described the physical properties and fabric changes in Yule marble deformed dry, at room temperature, under 10,000 atmospheres confining pressure. Taylor's hypothesis of homogeneous deformation was shown to be consistent with the observations. The high stresses, low temperature, and unnatural texture of the deformed material made it seem unlikely that these observations and this hypothesis would apply to naturally deformed marble. Accordingly, additional studies are being made in an attempt to approach more nearly the natural environment and phenomena. This paper reports the first step—an increase of temperature to 150°C, and the addition of interstitial water. All other conditions remain the same.

## ACKNOWLEDGMENTS

The experimentation was supported by a grant from the Office of Naval Research. The fabric studies were made possible by a grant from the Penrose Bequest of The Geological Society of America. Some of the pressure apparatus and the temperature-control equipment was built with the assistance of several grants from The Geological Society of America. Apparatus on loan from Harvard University and the U.S. Geological Survey was essential. The excellent craftsmanship of Mr. Fred Banning and Mr. Edwin Perry in the Institute of Geophysics Shop was indispensable. Mr. John de Grossé prepared his usual excellent thin sections. The Yule marble was provided by Mrs. E. B. Knopf out of whose inspiration this program has grown.

#### EXPERIMENTS

#### Apparatus

The apparatus used in these experiments is identical in principle and similar in design to that described in Part I. The high-pressure cylinder containing the specimen is heated by an external furnace, and is designed to minimize temperature gradients insofar as practicable. The temperature is controlled by a thyratron regulator, using a separate resistance winding as a sensing unit. The temperature of the cylinder is measured by a thermocouple deep in the cylinder wall. The difference between the cylinder temperature and the specimen temperature was determined in a mock-up at low pressure, with a second thermocouple in the place normally occupied by the specimen, and with all the rest of the apparatus the same. This difference is  $8^{\circ}$ C at  $150^{\circ}$ C,  $15^{\circ}$ C at  $300^{\circ}$ C. During a run the cylinder temperature varies less than  $1^{\circ}$ C on the average.

The specimen assembly is identical to that described in Part I. Pressure, force, friction, and piston displacement are measured, calibrated, and reduced as described in Part I. Experimental accuracies are about the same, but the reproducibility of the stress-strain curves is not so good. The average deviation from the mean is about 5 per cent as compared to 3 per cent in Part I. This is supposed to be due to the greater importance of undetermined variations in friction on these weaker specimens.

## Procedure

The assembly is first brought to the operating pressure, then heated. Two hours is required for the cylinder to come to thermal equilibrium. The test run is then made as described in Part I, either in extension or compression. The pressure is then reduced and the furnace turned off. Cooling takes about 2 hours. The whole run thus takes about four times as long as a room-temperature test.

For tests with interstitial water, the copper jacket is soldered to the two end pieces (see Part I, Fig. 2) leaving a small vent hole. The assembly is then filled with water (or other fluid) under vacuum, and the vent soldered shut. Since some water boils off while the vent is being soldered, there is no means of determining the exact amount of water before an experiment. After an experiment the specimen is removed from its jacket and weighed immediately. It is then heated to 150°C for 3 hours to evaporate the water, and weighed again. The difference in weight is taken to be the weight of the interstitial water present. Subsequent heating for longer periods showed no further change in weight.

Since the amount of water present, and hence its pressure under the test conditions, cannot be accurately determined in advance, it is generally impossible to perform extension tests with water present. When the water pressure exceeds the difference between the confining pressure and the longitudinal stress, the end

1386